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**Ulf Griesmann** National Institute of Standards and Technology Physical Measurement Laboratory Gaithersburg, Maryland 20899-8223 E-mail: guandou.wang@nist.gov **Abstract.** We describe a simple bilayer photoresist that is particularly well suited for laser lithography at an exposure wavelength of 405 nm on glass substrates, which are often used for the fabrication of binary diffractive optics and computer-generated holograms. The resist consists of a poly-dimethyl glutarimide (PMGI) bottom layer that is used as an antire-flection coating between a glass substrate and a positive or negative photoresist. The optical properties of the PMGI layer at 405 nm result in excellent suppression of reflections into the photoresist and good process latitude. © *The Authors. Published by SPIE under a Creative Commons Attribution 3.0 Unported License. Distribution or reproduction of this work in whole or in part requires full attribution of the original publication, including its DOI.* [DOI: 10.1117/1.OE.52.10.105104]

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#### 1 Introduction

Optical systems somtimes require components that are made with photolithography on glass substrates. Photomasks for projection or contact lithography are perhaps the most prominent examples. Photomasks are a specialized form of optical elements known as diffractive optics or computer-generated holograms (CGHs), which are fabricated using lithographic patterning technologies. CGHs are now used in many applications to shape and modify optical wavefronts.<sup>1,2</sup>

In many cases, the fabrication process for CGHs takes a cue from the entrenched fabrication process for semiconductor lithography photomasks. The hologram is fabricated by patterning a chromium layer on a glass substrate.<sup>3–8</sup> The result is a binary amplitude hologram with transparent and opaque fringes. A binary amplitude hologram can be converted into a binary phase hologram by etching the area of the glass substrate that is not covered by the chromium mask using a reactive ion etching (RIE) process followed by removal of the chromium layer. In this paper, we revisit this fabrication process for CGHs and describe an alternative process that is simpler than the established chromium-onglass process, performs better with high numerical aperture (NA) photolithography tools, and offers greater process flexibility.

#### 2 Bottom Antireflection Layers

CGHs are frequently fabricated using maskless laser lithography tools, which use optics with increasing NA to enable the writing of patterns with smaller and smaller feature sizes. For example, the zone plate array lithography (ZPAL) tool<sup>9,10</sup> in the Nano-Structured Optics Laboratory at the National Institute of Standards and Technology (NIST) uses arrays of beamlets with NAs of 0.6 or 0.8 to achieve feature sizes down to ~400 nm for the NA = 0.6 lenses and ~200 nm for the NA = 0.8 focusing lenses. The exposure wavelength is 405 nm, the wavelength emitted by high-power galliumnitride solid-state lasers, which are now used in many maskless laser lithography tools. With decreasing feature size, tight control of the lithography process is required. It is especially important to suppress the reflection of light into the photoresist film at the resist–substrate interface. Optical interference of light in the resist film otherwise results in uneven resist exposure and poor feature dimension control.<sup>11</sup>

Figure 1 shows a cross-section through a chromium-onglass photomask. When a chromium layer is patterned with lithography, suppression of the reflection by the chromium layer is clearly important because of the high refractive index of chromium and the resulting high reflectivity at a chromium-resist interface. Chromium layers are typically  $\sim$ 80 nm thick. We discuss different types of bottom antireflection coating (BARC) between the resist and chromium layers in this paper. Conventional photomasks are often made with a chromium oxide (CrO) antireflection layer to attenuate the reflection of light from the chromium layer into the resist.<sup>12</sup> Advanced photomasks use organic ARCs that achieve lower reflectivity.<sup>12</sup> Organic coatings are also useful when substrates are prepared on a small scale in a laboratory setting because they can be applied using a simple spin-coating process.

The effect of a BARC between the chromium and the photoresist on the reflection of light into the photoresist layer is shown in Fig. 2. The figure shows the reflectivity into the resist at 405 nm for a CrO ARC and also for two commercially available organic BARCs, BARLi and WiDE, as a function of BARC thickness. The reflectivity was calculated using Snell's law and the Fresnel equations at each material interface with the well-known transfer matrix method (see, e.g., Ref. 13). The reflectivities for s- and p-polarized light were averaged. Refractive indices and extinction coefficients for the polymer materials were measured at NIST using ellipsometry (with the exception of the data for the WiDE coating, which were provided by the supplier). Data for the refractive index of the borosilicate float glass that we used as a substrate material were available from the manufacturer (Schott BOROFLOAT 33, Schott, Germany). The refractive index of chromium at our wavelength of interest has been published.<sup>14</sup>



Fig. 1 Material stack on a photomask blank with a bottom antireflection coating.

The reflectivity of the photoresist-BARC interface was calculated for a set of angles of incidence with a 0.5 deg spacing between normal incidence and the maximum angle of incidence. The reflections at the glass substrate back surface and at the resist top surface were ignored in the calculations. Figure 2 shows the reflectivities for normal incidence (dotted lines) and for the maximum angle of incidence in a focused beam with NA = 0.6 in air (solid lines). The maximum angle of incidence inside a resist layer with a refractive index of 1.71 for an NA = 0.6 beam is close to 20 deg. The shaded areas indicate the range of reflectivities that are obtained at all angles between normal incidence and the maximum angle at a given BARC thickness. The CrO coating reduces the reflectivity into the resist from  $\sim 60\%$  for a chromium-resist interface without antireflection layer to  $\sim 1\%$ . Figure 2 also shows the reflectivity that can be achieved on chromium layers with two commercially available organic BARC materials (BARLi and WiDE).

BARC materials that are easily available commercially are optimized for an exposure wavelength of 365 nm (i-line) and are typically intended to be used on silicon, which has a much larger refractive index in the ultraviolet than chromium. It is therefore not surprising that the performance of these materials as antireflection layers on chromium is somewhat disappointing. With the BARLi BARC, it is at best possible to reduce the reflectivity at the bottom of the resist layer to ~0.5%. Exposure tests that we made with the ZPAL lithography tool at NIST showed that it was difficult to obtain good exposures on chromium layers with the commercial BARC materials.

We found that lithographic patterning of glass substrates is best done by patterning the glass without the use of a



Fig. 2 Reflectivity into the photoresist in a chrome-on-glass photomask for different types of antireflection layer.



**Fig. 3** Reflectivity into the photoresist for a glass substrate and a photoresist with n = 1.71 with different types of antireflection layer.

chromium layer. The reflectivity of a glass-resist interface is  $\sim 0.5\%$ , as can be seen in Fig. 3. The reflectivity is much lower than that of the resist-chromium interface, but we found that it is not sufficiently low to avoid noticeable interference effects. In our search for a suitable material for an antireflection layer, we discovered that an index matching layer of a readily available lift-off resist based on a polydimethyl glutarimide (PMGI) polymer results in excellent suppression of reflected light. The reason is a fortuitous coincidence: the refractive index of the PMGI layer at 405 nm(1.61) is close to the geometric mean of the refractive indices of the glass substrate (1.59) and the photoresist (1.71), which results in near-perfect suppression of the reflection by a quarter-wave antireflection layer.<sup>13</sup> The reflectivity into the photoresist of a PMGI layer on a borosilicate glass substrate is shown in Fig. 3, together with the reflectivity of the two commercial ARCs that are also shown in Fig. 2. The reflectivity for the PMGI layer has two minima close to  $10^{-4}$  at PMGI thicknesses of 60 nm (1/4 wave) and 190 nm (3/4 wave), at which it performs far better than the other ARCs.

Figure 4 shows a portion of a test grating with 500-nm wide lines written on a substrate made from borosilicate float glass that was coated with a bilayer resist consisting of 190-nm PMGI and  $\sim$ 400-nm positive photoresist. The test grating was written with the ZPAL lithography tool at NIST using beamlets with an NA of 0.6. The dark areas in Fig. 4 were exposed and the resist was removed during development.



**Fig. 4** Optical micrograph of 500-nm wide lines, written with a zone plate array lithography photolithography tool,<sup>9</sup> in 400-nm positive i-line photoresist with a 190-nm-thick layer of a poly-dimethyl glutarimide based lift-off resist as an antireflection layer on a borosilicate float glass substrate.

#### 3 Summary and Conclusions

We have demonstrated that a PMGI layer can be an excellent antireflection layer between a glass substrate and a photoresist for photolithography at 405 nm with high-NA laser lithography tools. PMGI polymers are widely used as resist materials for deep-ultraviolet lithography, electron-beam lithography, and also as a material for lithographic "lift-off" processes.<sup>15</sup> They are readily available as spin-on materials in a range of formulations. Using a PMGI layer as index matching layer between a glass substrate and photoresist has several advantages over conventional chromium-on-glass material stacks for the fabrication of diffractive optics and CGHs. A PMGI bottom ARC also provides good process latitude. Figure 3 shows that the reflectivity for a beam with NA = 0.6 remains below  $10^{-3}$  for a large range of coating thicknesses between 180 and 205 nm; precise thickness control and coating uniformity are therefore not critical. The PMGI polymer is soluble in water-based alkaline developers and is removed during the development process together with the photoresist. With a PMGI thickness of 190 nm and a photoresist thickness between 300 and 400 nm, the total thickness of the resist layer is between 500 and 600 nm. Phase profiles with a range exceeding  $2\pi$  can be etched into the glass substrates using an RIE process for all visible wavelengths because the etch rate of glass is approximately three times that of the polymer resist. The erosion of resist walls during the etching process can, potentially, result in a widening of lines that are etched into the glass substrate. This effect can be minimized by careful optimization of the etching process.<sup>16,17</sup>

For the fabrication of amplitude holograms, the same bilayer resist can be used, except that the order of metal coating and lithography are now reversed. The metal layer is deposited on the glass substrate after exposure and developing, and the resist is then removed (lifted off). In this way, wet etching of the metal layer is avoided, which is a process step that can be difficult to control in a laboratory setting. A more important advantage is that any metal can be deposited without the need to adapt the properties of the resist layers to the optical properties of the metal film.

A toolbox of functions for the calculation of optical multilayer properties, written in the GNU Octave language,<sup>18</sup> was developed to calculate the resist stack reflectivities. The toolbox and refractive index data are available from the authors upon request.

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Disclaimer: The full description of the procedures used in this paper requires the identification of certain commercial products and their suppliers. The inclusion of such information should in no way be construed as indicating that such products or suppliers are endorsed by NIST, or are recommended by NIST, or that they are necessarily the best materials or suppliers for the purposes described.

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